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# THE RELATION BETWEEN PLUMB-LINE DEFLECTION, GRADIENTS, AND RADII OF CURVATURE OF A GROUD

V. A. Kazinskiy

Summary: A method is given for deducing the formulas for studying the qeoidal surface with the aid of gradients of the terrestrial gravitational field.

1

We shall write two equations serving to determine the component plumbline deflections or deviations in the main planes: a and y, coinciding respectively with the morldian and the primary vertical (normal):

$$\mathcal{E}_{-} = \frac{T_{c}}{a}$$
,  $\eta = -\frac{T_{c}}{a}$  (1)

where  $T_x = \frac{dT}{dx}$  and  $T_y = \frac{dT}{dy}$  are the first derivatives of the disturbing potential T and g is the force of gravity at the surface of the geoid.

With the aid of these two equations, we shall find the analytical relation between: the component plumb-line deflections  $\xi$  and  $\eta$ , the second derivatives  $T_\Delta = \frac{d^2T}{dx^2} - \frac{d^2T}{dy^2}$  and  $Txy = \frac{d^2T}{dxdy}$ , and the radius of curvature t of the level surface of a geoid:

W(x, y, z) = 0

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Differentiating (1), respectively with respect to I and y, we obtain

where A is the azimuth of the element of length d:  $= \frac{1}{2} \cdot \frac$ 

If the first equation of (2) is multiplied by sin A and the second equation by cos A, then after subtracting one equation from the other we obtain:

atsin A - an cos A = 
$$T_{xy}^{(i)}$$
al, (3)

where

$$T_{XY}^{(1)} = \frac{1}{2} T_A \sin 2A + T_{XY} \cos 2A,$$
 (4)

hence, after integration, we obtain Edtvos equation:

$$(E_2 - E_1) \sin A - (\eta_2 - \eta_1) \cos A = \frac{1}{6} \int_{-\infty}^{\infty} T_{xy}^{(a)} d1,$$
 (5)

which finds application in the study of geoidal surfaces

III

. After the equations of (2) are multiplied respectively by cos A and sin A, we add them term by term. As a result of a not inconsiderable number of transformations, we obtain:

 $d = A + a \eta \sin A =$ 

$$= -\frac{1}{2} \sqrt{T_{xx}} \cos^2 A + T_{yy} \sin^2 A + RT_{xy} \sin A \cos A \int dl, \qquad (6)$$

honce, after integrating in the same interval as used previously, we obtain:

$$(\xi_{2} - \xi_{1}) \cos A + (\gamma_{2} - \gamma_{1}) \sin A =$$

$$= -\frac{1}{\pi} \int_{-\pi}^{\pi} T_{xx} \cos^{2} A + T_{yy} \sin^{2} A + 2T_{xy} \sin A \cos A / d1.$$
(7)

The equation just obtained above may be employed to determine the radius of curvature of a level surface of a geoid. Thus, it is sufficient to turn our attention to the nature of the integrand in function (7). It represents the negative quantity of the product of surface curvature  $(-\frac{1}{2})$  multiplied by the

acceleration of the force of gravity (g), that is to say it equals (2):

$$-\frac{\mathbf{g}}{\mathbf{g}} = \mathbf{T}_{\mathbf{x}\mathbf{x}} \cos^{2} \mathbf{A} + \mathbf{f}_{\mathbf{y}\mathbf{y}} \sin^{2} \mathbf{A} + 2\mathbf{T}_{\mathbf{x}\mathbf{y}} \sin \mathbf{A} \cos \mathbf{A}, \tag{8}$$

Consequently, instead of (6), we have:

d 
$$\not\in$$
 cos  $A + \underline{d}q$  sin  $A \Rightarrow \underline{1}$ .

d  $\overline{R}$ 

which gives, in the planes of the meridian and of the primary vertical (normal), the equalities:

$$\frac{35}{4} \frac{1}{R_{\rm M}} = \frac{2}{24} \frac{1}{R_{\rm N}} \tag{10}$$

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We note, for clarity, that  $R_h \neq -$  and  $R_N \neq N \neq -$  The expression (7) determines the deviation of the curvature of the geoid from the curvature of the surface of reference (deviation). Therefore, in order to obtain the complete curvature of a geoid, it is obviously necessary to calculate also the curvature of the surface, relative to which the geoidal surface is studied.

IV.

We return again to the equations in (2) and we set  $A=\infty + (A-\alpha)$ , where  $\alpha$  is the azimuth of the vector of plumb-line deflection  $E = \sqrt{E^2 + \eta^2}$ . Hence, for the case A = 0, we obtain:

$$d\mathcal{E} = -\frac{1}{g} \int_{\mathbf{x}x}^{\mathbf{T}_{xx}} + T_{xy} d\mathbf{g} \propto \int_{\mathbf{d}x},$$

$$d\eta = -\frac{1}{g} \int_{\mathbf{x}}^{\mathbf{T}_{yy}} + T_{xy} d\mathbf{g} \int_{\mathbf{d}y},$$
(11)

Hence, keeping in mind that :

$$dx = dx \cdot \cos \alpha$$
, and  $dx = dl \cdot \cos \alpha$ ,  $dy = dl \cdot \sin \alpha$ ,  $dy = dl \cdot \sin \alpha$ 

we obtain:

$$T_{xx} + T_{xy} t_g \alpha = T_{yy} + T_{xy} t_g \alpha. \tag{12}$$

Consequently,

$$tg^{\alpha} - ctg^{\alpha} = \frac{T_{\Delta}}{T_{xy}}, \quad \frac{a^{E}}{d\eta} = ctg^{\alpha}.$$
 (13)

Setting:

$$tg \propto - ctg \propto - \frac{2}{tg 2\alpha}$$
 (14)

we obtain:

$$tg \ 2\alpha = \underbrace{2T \ xy}_{T_{\Delta}} . \tag{15}$$

Equation (15) determines of in the direction of the plumb-line deflection  $\epsilon$  if  $T_\Delta$  and  $T_{XV}$  are known.

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